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A COMPUTERIZED METHOD OF PREDICTING ELECTRON BEAM  
BREMSSTRAHLUNG RADIATION WITH SPECIFIC APPLICATION  
TO HIGH VOLTAGE FLASH X-RAY MACHINES

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ABSTRACT

Many interesting phenomena occurring in the radiation output of large flash X-ray machines can be utilized only by understanding the action of the incident electron stream on the target. The detailed calculations required to understand these effects are best performed with a computer. This report explains the computer program utilized and tabulates the outputs obtained. The report also draws conclusions for future research, analysis, and machine design. Interrelationships were developed between the switch rise time, the radiation pulse length, the dose expected at 1 meter, and the dose distribution.

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## INTERRELATIONSHIPS BETWEEN RADIATION DOSES AT ONE METER AND MAIN SWITCH GAP RISE TIME IN LARGE FLASH X-RAY MACHINES

### Introduction

Many interesting phenomena occurring in the radiation output of large flash X-ray machines can be utilized only by understanding the action of the incident electron stream on the target. This involves detailed computations which can be performed only on a computer.

In November 1967, the dependence of the dose output at 1 meter on the angular distribution of electrons incident on the flash X-ray machine target was recognized to be a pertinent and somewhat neglected factor in the design of flash X-ray machines. A computer program to analyze flash X-ray machine outputs was written at Sandia Laboratories for use in the Hermes Program. The first results became available approximately February 1968. To date a general trend has been established for these calculations, and an insight into this problem has been developed which can be of value in future generator research and in the establishment of dose levels of experiments to be conducted on flash X-ray facilities.

### Computer Program

The computer program was written to operate on a RAX terminal for the IBM 360 computer. Figures 1 and 2 show the system analyzed. The target (A) was divided into 36 pie-shaped segments. One of these pie-shaped segments was then subdivided into six parts. A hemispherical dome, (B), was then placed above the target and divided into 10-degree segments. Eighteen planes, (C), were then defined along the Z axis which intersected the hemisphere's surface at 5-degree increments. The 10-degree segments on the sphere and the 5-degree increments are defined by the planes, so that the space above the target is divided into 648 points. Solutions for the radiation at these 648 points associated with each of the six target segments are obtained. After the radiation levels at the 648 points are defined, points are summed up by rotating one point into the other around the Z axis

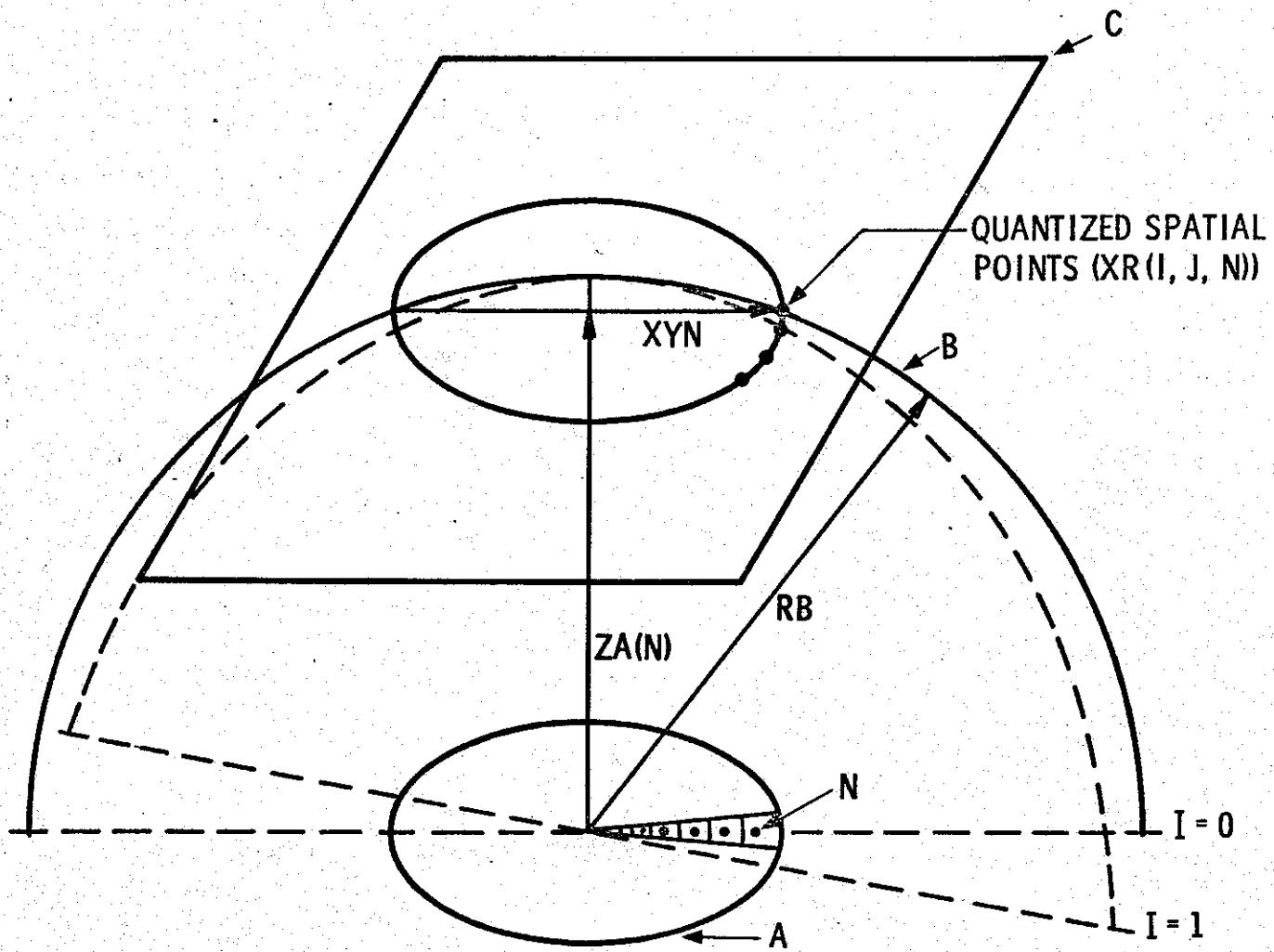


Figure 1. Geometry of Computer Solution

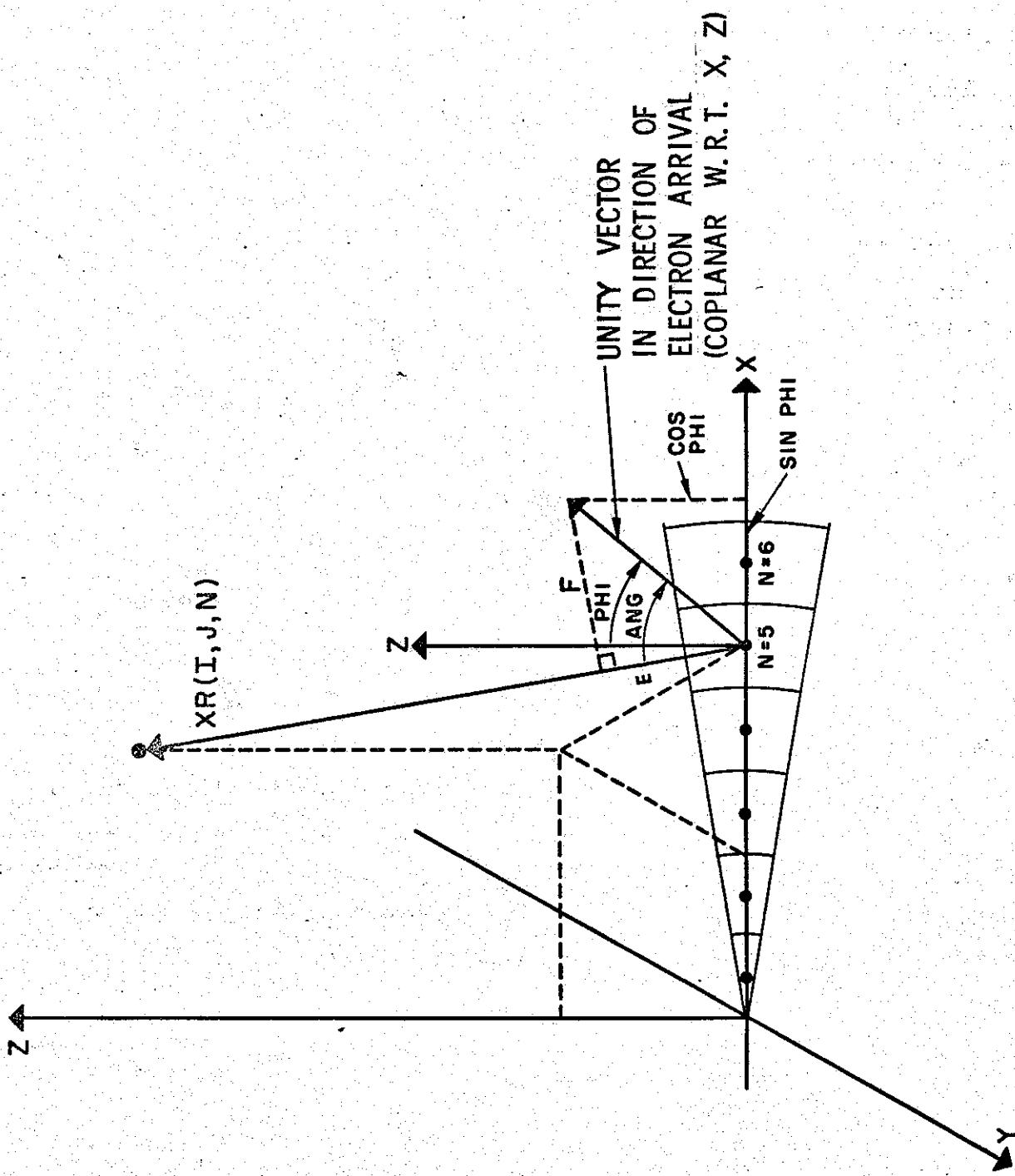


Figure 2. Vector Diagram of Electron Arrival Geometry

of the sphere. Thus, after 360-degree rotation, the six target segments are made to appear as the entire target. The radiation from the six target segments can be defined both in electron numbers and angle. The actual geometry used is shown in Figure 2.

#### Major Assumptions

Electron Beam Diameter -- It was assumed for this analysis that the spot size diameter was approximately equal to the number of megavolts between the anode and cathode multiplied times 1 inch per megavolt. Thus a 5-megavolt machine would have a 5-inch target diameter, and a 10-megavolt machine would have a 10-inch target diameter. This assumption is obviously open to question, but it has been valid for many of the machines at AWRE and for the machines at Sandia Laboratories. The spot size diameter will, in general, vary linearly with voltage in that the energy deposited on the target approximates a  $V^2$  relationship and the target area must increase as  $V^2$  or sustain damage. This assumption, if it isn't valid, can be easily modified in the program as better information becomes available.

Angular Distribution -- The normalized angular distribution of the radiation produced by electrons incident on a target was assumed to be a formula which is an average of the information available in the literature (References 1 and 2). This function was determined to be

$$F = e^{-\theta V / 0.667\pi},$$

where F is the intensity,  $\theta$  the angle in radians, and V in megavolts.

Divergence Angle -- It was assumed that divergence angle of the electron stream was a reasonably smooth function varying from approximately zero at a target radius of zero and then gradually increasing to achieve the average divergence angle which is used for the calculations in this paper. Results from Dr. Boers' computer program (Ref. 3) of Sandia Laboratories tend to indicate that this is not an accurate assumption in that the electrons closer to the center of the target may actually have a larger divergence angle than those on the periphery. However, this fact does not seriously affect the overall use of the computer output. This data can be modified to utilize trajectories available in the future.

Bremsstrahlung Production Efficiency Curve -- The curve used was the one proposed by Sandia. The Roentgens per coulomb equation is

$$R/Q = 1.1 \times 10^3 V^{2.8},$$

where V is in megavolts (Reference 4).

The actual computer program in FORTRAN language is included in Figure 3.

In order to obtain a uniform, slowly varying electron distribution on the target as a first approximation, straight lines were drawn from the anode to the cathode, and these lines were assumed to be the electron trajectories. The computer runs were then made by subdividing these angles so that the average angular distribution of the electrons could be programmed at 0, 5, 10, 15, and 20 degrees. Computations were also made where the angular distribution was constant across the target. For a constant electron beam arrival angle, the maximum intensity did not occur on axis but at the angle at which the electrons were distributed. Consequently, a constant angle of distribution was deemed as not representing any experimental bremsstrahlung distributions achieved to date. Computations were performed at 3, 4, 6, 8, 10, 12, and 15 and 20 MeV at 0, 5, 10, 15, and 20-degree average angles. The computer output consists of bremsstrahlung radiation intensity directly in front of the target on axis and at 5-degree increments from zero to 90 degrees. The program also normalizes the dose distribution to the dose on axis at zero degrees.

Analysis of the computer data is difficult since no one chart or graph can represent all of the information. One of the more complex factors that becomes evident is the changing spot size at voltages above 10 MV which causes apparent inconsistencies in almost all of the analyses. However, it is felt that this spot size is an important factor which should be taken into account. Since the prime information which is needed for flash X-ray machine analysis is the actual rads per coulomb plotted versus voltage, or the modified bremsstrahlung production efficiency, this important information was plotted. The plot for the actual bremsstrahlung production efficiency curve for various divergence angles is included as Figure 4. The important information is listed as follows:

1. With zero-degree divergence at a zero spot size, the modified bremsstrahlung production efficiency duplicates the bremsstrahlung production efficiency programmed on the computer.
2. The effect of large spot size drastically reduces the bremsstrahlung production at 1 meter.
3. The beam divergence angle causes extreme degradation of the modified efficiency curve. These efficiency curves can be used directly as a first approximation of bremsstrahlung output in designing new machines.

DC	- diameter of cathode target spot in meters
RN[N]	- radial distance to center spots of the 6 target sections
PA	- angles in radians to divide sphere into 18 sections in elevation
ZA(N)	- the intersection point on the Z-axis corresponding to planes intersecting the sphere at 5-degree increments
RB	- radius of sphere and/or distance from target at which computation is desired
XYN	- radius of circle formed by intersection of plane with the sphere
XA[N, I]	- X coordinate of plane N intersecting with longitude I.
YA[N, I]	- Y coordinate of plane N intersecting with longitude I
XR[I, J, N]	- distance from target segment n to XA[N, I] YA[N, I]. See Figure 2.
PHI(N)	- angle of electron arrival at target segment N in radians
C(N)	- equals sin (PHJ(N)). See Figure 2.
D(N)	- equals cos (PHI(N)). See Figure 2.
E	- See Figure 2
F	- See Figure 2
ANG	- determined by E, F above--angle between electron stream and XR(I, J, N) the observation point. Read in for six target points
G	- product of ANG(I, J, N) and megavolts
FE	- degradation due to angle represented by an equation using G as the input. Obtained by experiment.
RABN	- the inverse square distance degradation factor
RQ	- the rads at 1 meter per coulomb curve which also uses volts as an input
XCOL	- defined by input data
RELI(N)	- relative current density at target position N. Read in dist card for six positions
SCOL	- an operational unit
COL(N)	- the coulombs deposited on target section N
ARADS	- the radiation level at 1 meter from target section N
BRADS	- the radiation at point IJ on the sphere from all six target sections
RADS(I)	- the radiation at the 5-degree angles from all 216 target sections
TIME	- the pulse duration in seconds
V	- voltage in volts

Figure 3. List of Parameters and Program Used on Computer

```

/DISPLAY SV841
M.0073 ACTION IN PROGRESS.
L.0001 /JOP GO,TIME>10
L.0002 /FTC NAME>RAD
L.0003      DIMENSION RM[6], ZA[20],          XA[20,20], YA[20,20],
L.0004      1 C16], PH1[6], ANG[20,20,6], COL[6], FF[20,20,6],
L.0005      1 PHE[6], RELI[6], RADN[20],
L.0006      IRABNI[20,20,6], BRADS[20,20], RADS[20], ARADS[6], XR[20,20,6]
L.0007      1 ,D[6]
L.0008 C   RADN 1 METER FROM H2
L.0009      10 READ [9,2] V,AMPS, RB,          TIME
L.0010      READ [9,3] [PHE[N], N>1,6],[RELI[N], N>1,6]
L.0011      2 FORMAT [2E0.2/[E0.21]
L.0012      3 FORMAT [E0.2]
L.0013      PI>3.14159265
L.0014      DC>V*1.0E-6/39.37
L.0015      DO 101 N>1,6
L.0016      101 RM[N]>DC/12.0*[FLOAT[N]-0.5]
L.0017      DO 102 N>1,19
L.0018      PA>PI/36.0*[N-1]
L.0019      102 ZA[N]>RR*COS[PA]
L.0020      DO 104 N>1,19
L.0021      XYN>SQRT[RB**2-ZA[N]**2]
L.0022      DO 104 I>1,19
L.0023      XA[N,I]>XYN*COS[PI/18.0*[I-1]]
L.0024      104 YA[N,I]>XYN*SIN[PI/18.0*[I-1]]
L.0025      DO 105 N>1,6
L.0026      DO 105 I>1,19
L.0027      DO 105 J>1,19
L.0028      105 XR[I,J,N]>SQRT[[XA[I,J]-RN[N]]**2<YA[I,J]**2<ZA[I]**2]
L.0029      DO 106 N>1,6
L.0030      PH1[N]>PHE[N]/180.0*PI
L.0031      C[N]>SIN[PHE[N]]
L.0032      106 D[N]>COS[PHE[N]]
L.0033      DO 107 N>1,6
L.0034      DO 107 I>1,19
L.0035      DO 107 J>1,19
L.0036      E[XC[N]>XA[I,J]-RN[N]]<DE[N]*ZA[I]]/XR[I,J,N]
L.0037      F>SQRT[1.0-E**2]
L.0038      IF [E] 109, 207, 108
L.0039      108 ANG[I,J,N]>ATAN[F/E]
L.0040      GO TO 107
L.0041      207 ANG[I,J,N]>PI/2.0
L.0042      GO TO 107
L.0043      109 ANG[I,J,N]>PI-ATAN[ABS[F/E]]
L.0044      107 CONTINUE
L.0045      DO 110 N>1,6
L.0046      DO 110 I>1,19
L.0047      DO 110 J>1,19
L.0048      G>ABS[ANG[I,J,N]*V=1.0E-6]           1.0+EXP[-G/[0.667*PI]]
L.0049      110 FEI[I,J,N]>
L.0050      DO 111 N>1,6
L.0051      DO 111 I>1,19
L.0052      DO 111 J>1,19
L.0053      111 RABN[I,J,N]>1.0/XR[I,J,N]**2
L.0054      RQ>1.1F3*[V*1.0F-6]**2,8
L.0055      XCOL>AMPS*TIME
L.0056      TT>0.0
L.0057      DO 112 N>1,6
L.0058      112 TT*[2*N-1]*RELI[N]<TT
L.0059      DO 116 N>1,6
L.0060      SCOL>XCOL/[36.0*TT]
L.0061      116 COL[N]>SCOL*[2*N-1]*RELI[N]
L.0062      DO 117 N>1,6
L.0063      117 ARADS[N]>RQ*COL[N]
L.0064      DO 118 J>1,20
L.0065      DO 118 I>1,20
L.0066      118 BRADS[I,J]>0.0
L.0067      DO 111 N>1,6
M.0065 TRANSMISSION ERROR.
M.0065 TRANSMISSION ERROR.
L.0068      DO 113 I>1,19
L.0069      DO 113 J>1,19
L.0070      113 BRADS[I,J]>[ARADS[N]]*RABN[I,J,N]*FEI[I,J,N]<BRADS[I,J]
L.0071      DO 114 I>1,19
L.0072      114 RADN[I]>0.0
L.0073      DO 115 J>2,18
L.0074      DO 115 I>1,19
L.0075      115 RADN[I]>[BRADS[I,J]<RADN[I]]
L.0076      DO 216 I>1,19
L.0077      216 RADN[I]>2.0*RADS[I]<BRADS[I,I]<BRADS[I,19]
L.0078      WRITE [6,35] [RADN[I,I],I>1,19]
L.0079      DO 217 I>1,19
L.0080      217 RADN[I]>RADN[I]/RADN[I]
L.0081      WRITE [6,36] [RADN[I,I],I>1,19]
L.0082      36 FORMAT [8E15.5]
L.0083      GO TO 10
L.0084      35 FORMAT [8E15.5]
L.0085      END

```

Figure 3 (cont)

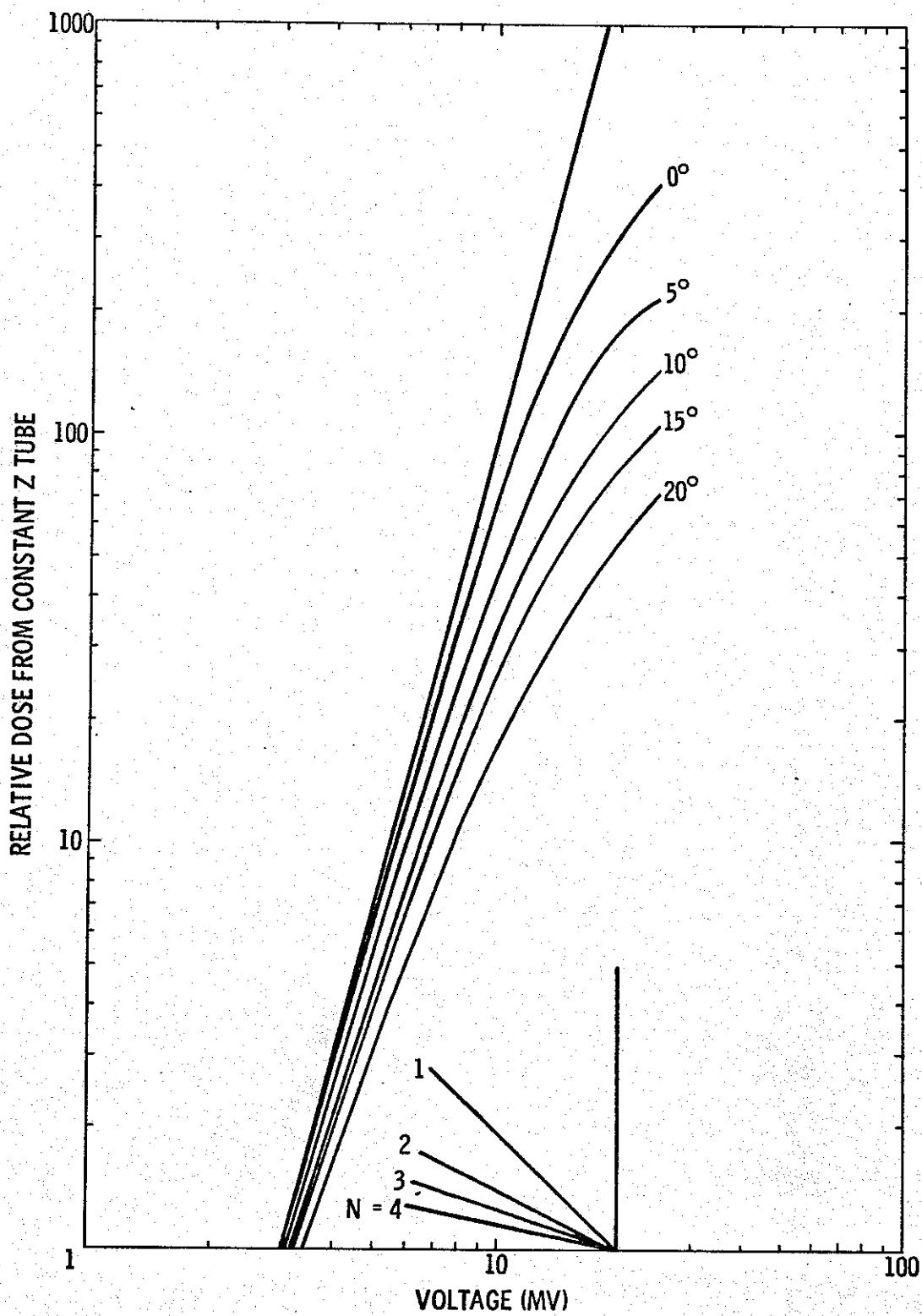
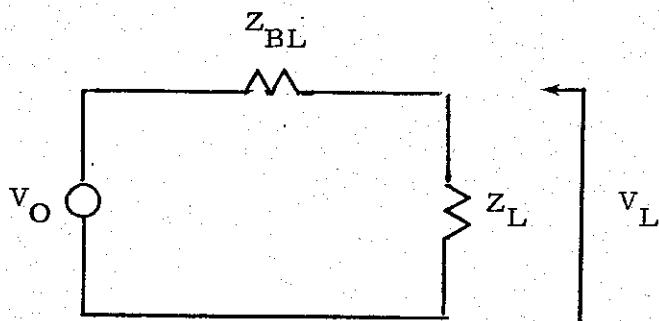


Figure 4. Summary of Computer Results

### Optimum Tube Impedance Derivation

The optimum way to design a flash X-ray machine would be to determine the bremsstrahlung production efficiency at a given voltage and then make the tube impedance  $n - 1$  times the impedance of the Blumleins. This derivation is shown below:



Assume that there is bremsstrahlung radiation emanating which is given as

$$\text{Output} = KV_L^{n-1} I,$$

where  $n - 1$  is the bremsstrahlung efficiency Roentgens per coulomb exponent:

$$I = \frac{V_L}{Z_L}$$

$$V_L = \frac{V_o Z_L}{Z_{BL} + Z_L}$$

$$\text{Output} = K V_o^n Z_L^{n-1} (Z_{BL} + Z_L)^{-n}$$

$$\frac{d(\text{Output})}{d Z_L} = KV_o^n \left[ (n - 1) Z_L^{n-2} (Z_{BL} + Z_L)^{-n} - n Z_L^{n-1} (Z_{BL} + Z_L)^{-n-1} \right].$$

Maximizing by equating to zero

$$0 = (n - 1)(Z_{BL} + Z_L) - n Z_L$$

$$= (n - 1)Z_B - Z_L$$

and

$$Z_L = (n - 1)Z_B$$

This means that if the bremsstrahlung production efficiency goes as  $V^4$  for a constant impedance tube then the X-ray tube impedance for maximum bremsstrahlung production at 1 meter should be three times the Blumlein impedance. This fact becomes more important in the machines operating between 10 and 20 MeV. If one looks at the newly generated efficiency curves, the conclusion can be reached that the bremsstrahlung production efficiency exponent rapidly decreases for large spot size and large angular distributions. Thus, for optimum bremsstrahlung production, the tube impedance can actually approach the matched condition or less, and a mismatched system is of value only when small distribution angles and small spot sizes are utilized.

#### Computer Results

The results of the computer runs are given in the appendix. Comparison of computer results with experiments conducted at voltages between 2 and 12 MeV on Sandia's Hermes flash X-ray machine have demonstrated excellent agreement in both the intensity and angular distribution. This will be detailed in a future report.

#### Voltage Rise Time Effects

The voltage output pulse from these machines can be reasonably described to a first approximation as two exponentials. The first starts at zero time and builds to a maximum value. After the voltage pulse time has elapsed, the other exponential will drop the voltage back towards zero. Ion Physics has generated a plot of the effect of various rise times in non-dimensional form. The pulse width divided by the switch rise time is plotted (Figure 5) versus the degradation in bremsstrahlung dose (Reference 1). The higher the exponential of the modified bremsstrahlung production efficiency, the worse the degradation from the switch rise time will be. Therefore, for a machine with either a large spot size or large electron beam divergence angle, the voltage rise time is a less important consideration in the

(Reference: Ion Physics DASA Proposal Contract DA-01-67C-0001)

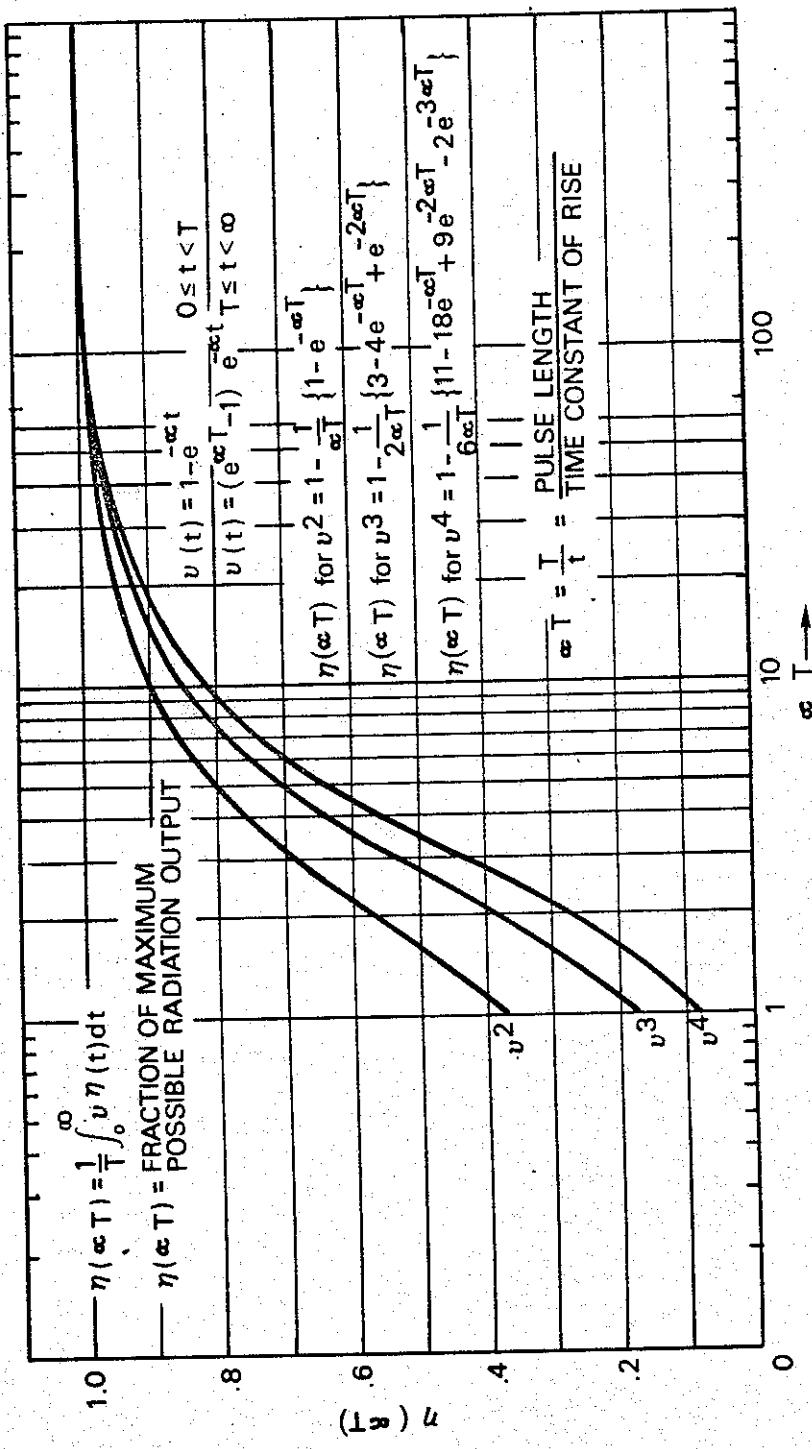


Figure 5. The Influence of Pulse Rise Time Upon System Efficiency

machine design. Simultaneous research needs to be conducted on the spot size, the beam divergence angle, and the rise time in order to obtain the maximum possible radiation dose in small volumes; the hypothesis set forth here has been verified in data obtained on large flash X-ray generators. For a 13-degree average electron beam divergence angle, the computer calculations predict that the bremsstrahlung production efficiency is proportional to the square of the voltage at 10 MeV. The radiation half intensity then occurs when the tube voltage reaches 0.707 of its peak value as predicted by the modified bremsstrahlung efficiency curve instead of 0.83 as predicted by the original efficiency curves; thus a longer radiation pulse results. This effect has been experimentally verified. This leads to the interesting conclusion that at voltages above 10 MV a good approximation to the beam divergence angle can be made by using the ratio of the bremsstrahlung production time half-width to the voltage pulse half-width.

#### Physical Interpretation

The following physical interpretation is presented in order to attach some reality and significance to the data obtained from the computer. At low voltage, the electrons yield bremsstrahlung radiation in almost isotropic distributions. At voltages above approximately 8 megavolts, the electron radiation sources are no longer isotropic but become highly directional. This is analogous to a flashlight bulb being utilized as the radiator for the lower voltages with a collimating reflector being moved into position behind the bulb proportional to the voltage. The higher voltage is analogous to a better collimated beam. The radiation or illumination half-angle will decrease, the on-axis intensity will increase, and the beam from the flashlight bulb will become a searchlight-type pattern where the inverse square law becomes invalid except for very large distances from the source. The reason for this is that when a point in the radiation field looks back at an extremely well-collimated source, the point can see only a small portion of the reflector or illuminator. In other words, since the radiation is so strongly collimated from other portions of the target, the point does not see these, and, consequently, no inverse square law can be obtained. This analogy also shows that dose distributions given in rads at 1 meter are meaningless for flash X-ray machine operation at about 8 MeV and above, in that a case could be hypothesized where an electron beam would be made converging and all the radiation would also converge at a point 1 meter from the target. This yields a maximum dose at that particular point only, and the intensity decreases in every direction. This converging beam, which requires

better beam control and handling methods than presently available, appears possible in the future.

### Conclusions

1. A computer program has been written for the IBM 360 computer which accurately predicts bremsstrahlung outputs in intensity and angle from large flash X-ray generators.
2. The long X-ray pulse width compared to the voltage pulse has been explained.
3. The interactions between voltage rise time, spot size, electron divergence angle, and bremsstrahlung dose output were derived.
4. From Figures 4 and 5, bremsstrahlung outputs from proposed flash X-ray machines can be accurately and quickly determined.

**APPENDIX**

COMPUTER PRINTOUT FORMAT

M 0077 ENTER DATA

VOLTAGE CURRENT

M 0077 ENTER DATA

DISTANCE FROM TARGET IN METERS RADS AT ONE METER

M 0077 ENTER DATA

PULSE WIDTH IN SECONDS-TIME

M 0077 ENTER DATA

ANGLES IN DEGREES FOR THE SIX TARGET SEGMENTS (FROM CENTER TO OUTSIDE) -- AVERAGE ANGLE

RELATIVE CURRENT INTENSITIES ON THE SIX TARGET SEGMENTS (FROM CENTER TO OUTSIDE)

Dose Values in Roentgens	{ 0 degrees 40 degrees 80 degrees	5 degrees 45 degrees 85 degrees	10 degrees 50 degrees 90 degrees	15 degrees 55 degrees 90 degrees	20 degrees 60 degrees	25 degrees 65 degrees	30 degrees 70 degrees	35 degrees 75 degrees
Relative Dose Normalized to 0 Degrees	{ 0 degrees 40 degrees 80 degrees	5 degrees 45 degrees 85 degrees	10 degrees 50 degrees 90 degrees	15 degrees 55 degrees 90 degrees	20 degrees 60 degrees	25 degrees 65 degrees	30 degrees 70 degrees	35 degrees 75 degrees

SIZE OF COMMON 00000 PROGRAM 47592

END-OF-COMPILEATION-RADS.

M.0077 ENTER DATA.

3.0E-2 RAD'S-AT-ONE-METER

1.0E-2 TIME

3.0E6 3.0F4

VOITS AND AIRS

M.0077 ENTER DATA.

1.0F0 RANS AT ONE MILE

M.0077 ENTER DATA.

3.0E-3 TIME

M.0077 ENTER DATA.

9.37 10.7 13.2 20.3 25.6 DEC ANC

M.0077 ENTER DATA.

1. 1. 1. 1. 1.

0.14695E 02 0.146730E 02 0.144251E 02 0.13419E 02 0.12347E 02

0.79410E -01 0.70527E -01 0.62351E -01 0.55511E -01 0.46192E -01

0.30119E 01 0.26567E 01 0.22550E 01 0.19543E 01 0.16535E 01

0.10000E 01 0.93945E 00 0.95673E 00 0.98093E 00 0.92326E 00

0.53448E 00 0.47458E 00 0.42089E 00 0.37295E 00 0.33026E 00

-0.20221E -00 -0.17837E -00 -0.15475E -00

M.0077 ENTER DATA.

3.0E6

VOITS AND AIRS

M.0077 ENTER DATA.

1.0E0 RANS AT ONE MILE

M.0077 ENTER DATA.

3.0E-3 TIME

M.0077 ENTER DATA.

2.29 7.40 12.5 17.6 22.7 27.8 30.0 DEC ANC

M.0077 ENTER DATA.

1. 1. 1. 1. 1.

0.12787E 02 0.12693E 02 0.12430E 02 0.12003E 02 0.11417E 02

0.79476E -01 0.71327E -01 0.63602E -01 0.55609E -01 0.46178E -01

0.30371E 01 0.26813E 01 0.22861E 01 0.20316E 01 0.39637E 01

0.10000E 01 0.99259E -00 0.97207E -00 0.94207E -00 0.83548E -00

0.62387E 00 0.55779E 00 0.49733E 00 0.42099E 00 0.39346E 00

0.24220E 00 0.20962E 00 0.17872E 00

M.0077 ENTER DATA.

1. 1. 1. 1. 1.

0.12787E 02 0.12693E 02 0.12430E 02 0.12003E 02 0.11417E 02

0.79476E -01 0.71327E -01 0.63602E -01 0.55609E -01 0.46178E -01

0.30371E 01 0.26813E 01 0.22861E 01 0.20316E 01 0.39637E 01

0.10000E 01 0.99259E -00 0.97207E -00 0.94207E -00 0.83548E -00

0.62387E 00 0.55779E 00 0.49733E 00 0.42099E 00 0.39346E 00

0.24220E 00 0.20962E 00 0.17872E 00



4.E6 4.E4 VMTS AND AMPA  
 H.0077 ENTER DATA.  
 1.0E0 RADs AT CLE-4FTFS  
 H.0077 ENTER DATA.  
 3.0E-8 TIME  
 H.0077 ENTER DATA.  
 1.72 5.55 9.37 -10.7 -13.2 -20.9 -15 DEG AIC  
 H.0077 ENTER DATA.  
 1. 1.  
 0.38947E 02 0.38437E 02 0.30095E 02  
 0.17405E 02 0.14890E 02 0.12665E 02  
 0.33003E 01 0.22043E 01 0.12432E 01  
 0.10000F 01 0.98690E-06 0.94898E 00  
 0.44688E 00 0.38155E 00 0.32518E 00  
 0.34740E-01 0.34995E-01 0.31921E-01  
 H.0077 ENTER DATA.  
 4.E6 4.E4 VMTS AND AMPA  
 H.0077 ENTER DATA.  
 1.0E0 RADs AT CLE-4FTFS  
 H.0077 ENTER DATA.  
 3.0E-8 TIME  
 H.0077 ENTER DATA.  
 2.28 7.46 12.5 17.6 22.7 27.6 22 DEG AIC  
 H.0077 ENTER DATA.  
 1. 1.  
 0.31922E 02 0.31043E 02 0.30830E 02  
 0.17735E 02 0.15291E 02 0.13118E 02  
 0.37137E 01 0.27495E 01 0.19322E 01  
 0.340020E 01 0.30126E 00 0.30760E 00  
 0.555557E 00 0.47922E 00 0.41093E 00  
 0.11633E 00 0.96131E-01 0.60528E-01



G. FE. .... G.F4.		UNITS AND DATA	
H. 0077 ENTER DATA.		WARS AT ONE HETTER	
I. 0077 ENTER DATA.		WARS AT ONE HETTER	
3.0E-8	TIME	3.0E-8	TIME
1. 72	5.55	9.37	16.7
4. 0077 ENTER DATA.		2C.4	1E-212 AM
1.	1.	1.	1.
0. 13786E-02	0.13577E-02	0.11282E-02	0.10342E-02
-0.45167E-02	-0.31798E-02	-0.22625E-02	-0.15264E-02
0. 0	0. 0	0. 0	0. 0
-0.10000E-01	-0.98480E-01	-0.94167E-01	-0.86235E-01
-0.31312E-01	-0.23000E-01	-0.16412E-01	-0.11164E-01
0. 0	0. 0	0. 0	0. 0
H. 0077 ENTER DATA.		W4TS AND AMPA	
4. 0077 ENTER DATA.		W4TS AND AMPA	
1. 0E0	1.0E0	1.0E0	1.0E0
I. 0077 ENTER DATA.		WARS AT ONE HETTER	
3.0E-2	TIME	3.0E-2	TIME
4. 0077 ENTER DATA.		2D.7	2D.7
2.29	7.40	12.5	17.6
H. 0077 ENTER DATA.		2D.7	2D.7
1.	1.	1.	1.
0. 10592E-05	0.10285E-05	0.10021E-05	0.95902E-05
-0.45047E-02	-0.34667E-02	-0.25980E-02	-0.18836E-02
0. 92332E-09	0. 0	0. 0	0. 0
-0.10000E-01	-0.98975E-01	-0.94341E-01	-0.82287E-01
0. 43349E-02	0. 33354E-02	0. 25091E-02	0. 18184E-02
0. 88852E-02	0. 0	0. 0	0. 0
H. 0077 ENTER DATA.		WARS AT ONE HETTER	
3.0E-2	TIME	3.0E-2	TIME
I. 0077 ENTER DATA.		WARS AT ONE HETTER	
1. 0E0	1.0E0	1.0E0	1.0E0
H. 0077 ENTER DATA.		WARS AT ONE HETTER	
3.0E-2	TIME	3.0E-2	TIME
I. 0077 ENTER DATA.		WARS AT ONE HETTER	

1.0077 ENTER DATA.

1.0050 RAD'S AT OUT METER

1.0077 ENTER DATA TIME

1.0077 ENTER DATA.

1.0077 FILTER DATA.

1.0000 RAD'S AT OUT METER

1.0050 RAD'S AT OUT METER

1.0077 ENTER DATA TIME

1.0077 ENTER DATA.

1.0050 RAD'S AT OUT METER

1.0077 ENTER DATA TIME

1.0077 ENTER DATA.

1.0050 RAD'S AT OUT METER

1.0077 ENTER DATA TIME

1.0077 ENTER DATA.

1.0050 RAD'S AT OUT METER

1.0077 ENTER DATA TIME

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1.0050 RAD'S AT OUT METER

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1.0050 RAD'S AT OUT METER

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1.0050 RAD'S AT OUT METER

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1.0077 ENTER DATA.

1.0050 RAD'S AT OUT METER

1.0077 ENTER DATA TIME

1.0077 ENTER DATA.

1.0050 RAD'S AT OUT METER

1.0077 ENTER DATA TIME

6.E6 E.E4 VOLTS AND AMP.

11.0077 ENTER DATA.

11.0077 ENTER DATA. RISE AT ONE HUNDRED

11.0077 ENTER DATA. TIME

11.0077 ENTER DATA.



H.0077 ENTER DATA. 10. F4 VOLTS AND AMPS

H.0077 ENTER DATA. RAD'S AT ONE 'HET'.

H.0077 ENTER DATA. TIME

H.0077 ENTER DATA.

1.72 5.55 9.37 10.7 13.2 23.3 15 DEC ANG

H.0077 ENTER DATA.

1. 1. 1. 1. 1.

0.10654E 04	0.10505E 04	0.10140E 04	0.09353E 03	0.79612E 02	0.63284E 03	0.48250E 03	0.33902E 03
0.23211E 03	0.15057E 03	0.10457E 03	0.09320E 02	0.45098E 02	0.28675E 02	0.19590E 02	0.12704E 02
0.82953E 01	0.53862E 01	0.34853E 01	0.26170E 00	0.86183E 00	0.74743E 00	0.59242E 00	0.45237E 00
0.10000E 01	0.96595E 00	0.95170E 00	0.65063E 01	0.42884E -01	0.26134E -01	0.18387E -01	0.11980E -01
0.21786E 00	0.14636E 00	0.92145E -01	0.32712E -02				
0.72559E -02	0.50502E -02						

H.0077 ENTER DATA.

10. F6 10. F4 VOLTS AND AMPS

H.0077 ENTER DATA.

1. 0E0 RAD'S AT ONE 'HET'.

H.0077 ENTER DATA. TIME

H.0077 ENTER DATA.

2.29 7.46 12.5 17.6 22.7 27.8 20 DEC ANG

H.0077 ENTER DATA.

1. 1. 1. 1. 1.

0.71027E 03	0.70243E 03	0.69952E 03	0.66820E 03	0.63349E 03	0.58303E 03	0.51139E 03	0.41441E 03
0.30013E 03	0.20911E 03	0.14258E 03	0.95279E 02	0.63833E 02	0.42177E 02	0.27702E 02	0.18102E 02
0.11793E 02	0.76567E 01	0.42602E 01	0.97902E 00	0.22228E 00	0.89115E 00	0.62018E 00	0.71928E 00
0.10000E 01	0.92812E 00	0.97902E 00	0.20585E 00	0.13488E 00	0.89795E 00	0.59331E -01	0.38969E -01
0.42220E 00	0.26415E 00	0.20585E 00	0.13488E 00	0.10771E -01	0.69777E -02		

H.0077 ENTER DATA.

/CANCEL ACTIVITY TERMINATED.

H.0072 BEGIN ACTIVITY.

-12.66 -12.E4

464.FC-AUD-AIPS

H.0077 ENTER DATA.

1.0E0

RADS AT ONE METER

-6.0E-6 TIME

H.0077 ENTER DATA.

H.0077 ENTER DATA.

1. 1. 1. 1.

6.47377E 04	0.42023E 04	0.30410E 04	0.19277E 04	0.11650E 04	0.73614E 03	0.44867E 03	0.27318E 03
0.16524E 03	0.16042E 03	0.60636E 02	0.36668E 02	0.22059E 02	0.17265E 02	0.73793E 01	0.47968E 01
0.18834E-04	0.17346E-04	0.10442E-04	0.10442E-04	0.10442E-04	0.10442E-04	0.10442E-04	0.10442E-04
0.10000E 01	0.29966E 00	0.64187E 00	0.46668E 00	0.25223E 00	0.15493E 00	0.34701E-01	0.57660E-01
0.35040E-01	0.21979E-01	0.12009E-01	0.77269E-02	0.46347E-02	0.28066E-02	0.16842E-02	0.10125E-02
0.60870E-03	0.36612E-03	0.22030E-03					

H.0077 ENTER DATA.

12.FC 12.E4

H.0077 ENTER DATA.  
1.0E0 RADS AT ONE METER  
6.0E-2 TIME

H.0077 ENTER DATA.

1.573 1.85 3.12 4.4 5.67 6.95 7.5 EFC ANC

1. 1. 1. 1.	1. 1. 1. 1.	0.25637E 04	0.19325E 04	0.12177E 04	0.83577E 03	0.51836E 03	0.31980E 03
0.19520E 03	0.11846E 03	0.71523E 02	0.63018E 02	0.25787E 02	0.1641CE 02	0.61950E 01	0.54755E 01
0.32569E-01	0.19562E-01	0.11560E-01	0.84160E 00	0.45099E 00	0.27642E 00	0.17071E 00	0.10501E 00
0.10000E 01	0.65663E 00	0.38691E-01	0.23463E-01	0.14125E-01	0.84677E-02	0.50661E-02	0.20192E-02
0.15094E-02	0.93575E-03	0.37790E-03					

H.0077 ENTER DATA.

12.FC 12.E4

H.0077 ENTER DATA.  
1.0E0 RADS AT ONE METER  
6.0E-2 TIME

H.0077 ENTER DATA.

1.15 3.70 6.25 8.8 11.35 13.9 16.06 ANC

1. 1. 1. 1.	1. 1. 1. 1.	0.19629E 04	0.18756E 04	0.16745E 04	0.15759E 04	0.14768E 04	0.13752E 04
0.20318E 04	0.15232E 03	0.92457E 02	0.55723E 02	0.32357E 02	0.17130E 02	0.91346E 01	0.70033E 01
0.24872E 03	0.24623E 01	0.16532E 01	0.92351E 01	0.57231E 01	0.32357E 01	0.18346E 01	0.10751E 01
0.61409E 01	0.97246E 00	0.62351E 00	0.37231E 00	0.22351E 00	0.132351E 00	0.77577E 00	0.477577E 00
0.10000E 01	0.74565E-01	0.45565E-01	0.27665E-01	0.16665E-01	0.10665E-01	0.6665E-01	0.40136E-01
0.12241E 00	0.12020E-02	0.76110E-02	0.45565E-02	0.27665E-02	0.16665E-02	0.10665E-02	0.24444E-02

12. FG 12. F4

VOLTS AND AMPS

H.0077 ENTER DATA:

1.0E0

RADS AT ONE LETTER

6.0E-2 TIME

H.0077 ENTER DATA:

1.72 5.55

10.7 13.2

20.9 15 DEC A/M

H.0077 ENTER DATA:  
1. 1. 1.  
0.15725E-04 0.15520E-04 0.15166E-04  
0.31026E-03 0.19325E-03 0.11556E-03  
0.53504E-01 0.31441E-01 0.18441E-01  
0.10000E-01 0.28750E-00 0.90410E-00  
0.19732E-00 0.12290E-00 0.75398E-01  
0.3402CE-02 0.19394E-02 0.11723E-02

H.0077 ENTER DATA:  
12. FG 12.F4  
VOLTS AND AMPS  
H.0077 ENTER DATA:  
1.0E0 RADS AT ONE LETTER  
6.0E-2 TIME

H.0077 ENTER DATA:  
2.29 7.40 12.5 17.6 22.7 27.8 20 DEC A/M  
H.0077 ENTER DATA:  
1. 1. 1.  
-0.10138E-04 -0.99992E-03 -0.98780E-03  
0.44707E-03 0.29071E-03 0.18304E-03  
0.66251E-01 0.50051E-01 0.25557E-01  
0.10009E-01 0.98632E-00 0.97427E-00  
0.44099E-02 0.26676E-02 0.16367E-02  
0.85078E-02 0.49963E-02 0.25254E-02

15.E6 15.E4 VOLTS AND AMPS

H.0077 ENTER DATA 1.0E0

RADS AT ONE DEGREE

6.0E-8 TIME

H.0077 ENTER DATA

4.0E-8 TIME

H.0077 ENTER DATA

1.0E0

RADS AT ONE DEGREE

6.0E-8 TIME

H.0077 ENTER DATA

1.0E0

RADS AT ONE DEGREE

6.0E-8 TIME

H.0077 ENTER DATA

1.0E0

RADS AT ONE DEGREE

6.0E-8 TIME

H.0077 ENTER DATA

1.0E0

RADS AT ONE DEGREE

6.0E-8 TIME

H.0077 ENTER DATA

1.0E0

RADS AT ONE DEGREE

6.0E-8 TIME

H.0077 ENTER DATA

1.0E0

RADS AT ONE DEGREE

6.0E-8 TIME

H.0077 ENTER DATA

1.0E0

RADS AT ONE DEGREE

6.0E-8 TIME

H.0077 ENTER DATA

1.0E0

RADS AT ONE DEGREE

6.0E-8 TIME

H.0077 ENTER DATA

1.0E0

RADS AT ONE DEGREE

6.0E-8 TIME

H.0077 ENTER DATA

1.0E0

RADS AT ONE DEGREE

6.0E-8 TIME

1. 1. 1. 1. 1.

0.75503E-04	0.51130E-04	0.33245E-04	0.18581E-04	0.10103E-04	0.55153E-03	0.29043E-03
0.44520E-02	0.23475E-02	0.12345E-02	0.6782E-02	0.33972E-01	0.17812E-01	
0.25895E-00	0.125895E-00	0.62146E-00	0.40320E-00	0.22547E-00	0.12152E-00	0.66922E-01
0.91615E-01	0.46223E-01	0.22847E-02	0.11170E-02	0.74221E-02	0.41221E-02	0.21613E-02
0.11342E-03	0.55623E-04	0.31121E-04				

1. 1. 1. 1. 1.

0.47418E-04	0.47418E-04	0.47418E-04	0.34218E-04	0.22418E-04	0.12494E-04	0.72355E-03
0.21219E-03	0.11218E-03	0.59503E-02	0.31141E-02	0.16190E-02	0.83037E-01	0.43228E-01
0.58607E-00	0.30112E-00	0.22541E-00	0.10790E-00	0.69571E-00	0.45640E-00	0.26231E-00
0.11401E-01	0.55214E-01	0.22947E-01	0.12098E-01	0.63314E-02	0.32933E-02	0.17037E-02
0.23210E-03	0.11316E-03	0.61223E-04				

1. 1. 1. 1. 1.

0.49184E-04	0.49184E-04	0.49184E-04	0.34218E-04	0.22418E-04	0.12494E-04	0.72355E-03
0.21219E-03	0.11218E-03	0.59503E-02	0.31141E-02	0.16190E-02	0.83037E-01	0.43228E-01
0.58607E-00	0.30112E-00	0.22541E-00	0.10790E-00	0.69571E-00	0.45640E-00	0.26231E-00
0.11401E-01	0.55214E-01	0.22947E-01	0.12098E-01	0.63314E-02	0.32933E-02	0.17037E-02
0.23210E-03	0.11316E-03	0.61223E-04				

1. 1. 1. 1. 1.

0.31139E-04	0.30512E-04	0.26242E-04	0.23501E-04	0.21034E-04	0.10490E-04	0.57690E-03
0.16910E-03	0.91088E-03	0.51088E-02	0.31010E-02	0.21473E-02	0.12581E-02	0.52691E-01
0.23025E-00	0.12522E-00	0.63534E-00	0.33010E-00	0.16155E-01	0.76495E-02	0.32576E-00
0.10000E-01	0.57906E-01	0.28534E-01	0.14581E-01	0.73010E-02	0.38010E-02	0.18402E-00
0.10161E-03	0.54581E-04	0.27644E-04	0.13848E-04	0.71615E-05	0.34495E-02	











#### LIST OF REFERENCES

1. Nablo, Lincox, Stewart, Weisman, "Presentation of Study Results Leading to the Definition of a Super Flash X-Ray Facility," Ion Physics Corporation, Contract DA-01-676-0001, Figures 4-6.
2. Unpublished Private Communication, Physics International Company.
3. Report to be Published, J. E. Boers, Sandia Corporation. *Mathematics Note 12*
4. Report to be Published, T. H. Martin, Sandia Corporation.